Edge Localised Modes: ELMs

J W Connor Culham Science Centre Abingdon, UK

ITER School Aix-en-Provence, France July 2007

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ELMs

- What are they?
- Why do they matter?
- What causes them?
- Can we control them?

History: L and H-modes

- Adding external heating power to Ohmically heated tokamaks produced L-mode discharges with degraded confinement
- Serendipitously, ASDEX showed a sudden transition to the higher confinement H-mode above a certain threshold power, P_{L-H}
 - since found in all tokamaks with $P > P_{L-H}$
- The H-mode has steep edge gradients associated with an edge transport barrier giving improved confinement

Evolution of Edge Density Profile (ASDEX)



Edge Pedestal (JET) n_e, T_e, T_i





Fig. 4.3. Radial edge profiles of electron density and electron and ion temperature taken from interferometry, edge LIDAR, CXSE and ECE. Fits of hyperbolic tangent functions to the electron density and temperature data are shown as a solid line. (From Ref. [116].)

Fig. 4.1. Electron temperature profile measured with the ECE heterodyne radiometer. This profile was taken during the stationary phase of an ELMy H-mode (pulse #44012, 14 MW NBI), in-between two Type I ELMs. The closed circles indicate the experimental points and the open square the extrapolated position of the edge pedestal. (From Ref. [11].)

Schematic Profile



ITER Baseline Scenario - Plasma



ELMs

- However this was accompanied by instabilities at the plasma edge: ELMs
- Short bursts ejecting edge plasma
- Remove impurities and help control plasma density
- BUT can trigger large MHD events
- AND cause unacceptable erosion on divertors

ELM Heat Losses rapidly eject heat and particles



- Steep gradients drive instability
 - Pressure helps overcome magnetic containment
 - Peels off edge of plasma & drops gradients
 - Energy dumped outside plasma:
 - carried along field lines to divertor



ELMs Ablate the Divertor Tiles

- Ablation process rises sharply above a threshold in energy
 - note for ITER: energy goes as (size)³ while tile area
 ∞(size)²





1MJ ELMs lead to strong ablation and so high radiation

0.5MJ ELMs lead to minimal ablation and so low radiation Outline of ELM Characteristics

ELM Characteristics

- D_{α} (H_{α}) trace \implies periodic enhanced plasma wall interaction
- Different types: Type I, Type III etc (later)
- Magnetic signals on Mirnov coils as 'precursors' MHD instability?
- Periodic loss of plasma in edge pedestal

 ⇒ fluctuation-enhanced losses
- Fast electrons at divertor reconnection?

D_{α} Traces (JET): Types I & III



Fig. 4.7. Time traces of the D_{α} emission from the outer divertor region for five discharges in a density scan at 2.5 MA/2.7 T, δ =0.47. The pulses are in order of increasing gas fuelling with the lowest fuelling in the uppermost box. All discharges are NBI heated with a high power flat of 13.5 - 15 MW beginning at ≈17 seconds and extending to ≈20 seconds for #52308 and beyond 22 seconds for the rest. The discharge number is given for each box along with the mean Type I ELM frequency during the main Type I or Type I-II ELMy H-mode phase. (From Ref. [13].)

Magnetic Signals

MHD Characteristics of ELMs on ASDEX Upgrade



Type III ELM exhibits magnetic precursor

- υ = 75 kHz, m \approx 10, very edge localized (< 4 cm)

- Type I ELM has no (detectable) magnetic precursor for
- Type I ELM precursor on ECE for co.
- either electrostatic or very high m (> 20)
- Transport during type I ELM turbulent

ELM Effect on Stored Energy (JET)



Fig. 4.8. Comparison of the D_{α} emission from the outer divertor region for two of the pulses in Fig. 4.7 (box 1 and 2). The respective total plasma stored energies (box 3, taken directly from the diamagnetic measurement) and line average densities (box 4) are also shown. The dashed line in box 4 represents the Greenwald density limit.

Effect of ELM Frequency on Confinement

CONFINEMENT AND LOSSES Degradation of τ_E

• $\tau_E^{ELMyH} \simeq \eta \tau_E^{ELM-freeH}$: $\eta \simeq 0.85$

Physics basis (Zohm) $\eta = 1 - \left[1 - \left(\frac{r_{ELM}}{a}\right)^{2}\right] \frac{f_{ELM}\delta W}{P}$ • H-factor $H \equiv \frac{\tau^{H}}{\tau^{L}}$ JT-60U $I_{L} = \frac{\tau^{H}}{1.5}$ $I_{L} = \frac{1}{2}$ $I_{L} = \frac$

Energy Confinement v ELM Frequency

Energy confinement time and ELM frequency

From Fishpool, Nucl Fusion 38, 1373 (1998).

H89 and H93 confinement enhancement on JET



Confinement in ELMing Regimes (JET)



Fig. 2.13. Consistency of the energy confinement with the IPB98(y,2) scaling. $H_{IPB98(y,2)} = \tau_E / \tau_{IPB98(y,2)}$. Data is taken from gas fuelled, NBI and ICRH heated, JET stationary ELMy H-modes from 1994-2001 (red crosses for Type I ELMy Hmodes, blue circles for Type III ELMy H-modes) with three dedicated β scans overlaid. Each scan is represented by a different symbol (purple diamonds, black squares or orange circles) and has different values of ρ^* and ν^* , for a range of β .

Filaments



 $\frac{\Phi_{toroted}(^{\circ})}{100 \ 150 \ 200 \ 250 \ 300 \ 350 \ 400 \ 45c} = \frac{-0.3 \ \text{Linearization of the structure}}{-3 \ -2 \ -1 \ 0}$ MAST: clear evidence for filaments during ELMs (*Kirk, et al 2004*) $\frac{\Phi_{toroted}(^{\circ})}{100 \ 150 \ 200 \ 250 \ 300 \ 350 \ 400 \ 45c} = \frac{-0.3 \ \text{Linearization of the structure}}{-3 \ -2 \ -1 \ 0}$ Eich, poster 2.6 ASDEX-Upgrade: stripes on target plate and structures in TS consistent with flux bundles



DIII-D: filaments detected in CIII emission (*Fenstermacher*, 2004)

structures in TS consistent with flux bundles ejected from core (*Eich, et al 2004/2005, Kurzan, 2005*)



Filament associated with small Type V ELM on NSTX. (*Maingi, et al* 2005)



SOL Structure: MAST

• Images taken of MAST "spherical tokamak" with fast visible camera (A. Kirk, S. Lisgo, UKAEA)



Filaments in JET Slow visible camera images

- can see footprint of helical flux tubes (first reported by Ph. Ghendrih PSI 2002)

69481 various ELM's



Viewed from Octant 4

Viewed from Octant 8

JET Fast Visible Camera

Reference view of vessel



CIEMAT diagnostic

Ref to A. Alonso's EPS poster



A ~ 1MJ ELM, recorded at 3000 frames/s (clip covers 100msec)

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ELMing H-Mode

Regimes

ELM Types

- Type I ELMs
- Type II ELMs
- Type III ELMs
- Type IV ELMs
- Type V ELMs
- Grassy ELMs

Type III and Type I ELMs

MAST



Time (s)

Operating Diagram



Type III ELMs

- Higher ELM frequency
- Smaller energy loss per ELM
- Reduced confinement (10 30 %)
- Type III ELMs are observed below a critical pedestal

temperature



T_{crit} tends to increase with toroidal field

Type III ELMs



The low n_e-high T_e branch of Type III was originally called type IV

Whether Type III ELMs at low and high collisionality are due to the same physics mechanism is still an open question

Precursors to Type III ELMs

Type III : more clearly associated with precursors

	п	т	Δr (cm)	f(kHz)	$\tau(\mu s)$
JET DIII-D	≥ 8 5 – 10 (low n_e 6-13)		10	50-100 (multiple 50-80)	250
ASDEX Upgrade C-MOD	10-15 > 5	15-20 > 10	4	100 (counter) 60 (co); sometimes 2 modes 100, 200 150	≤ 50
COMPASS-D		13		70-120	≤ 200
TCV JFT-2M	5-8			120 ↓ 70 250 ↓	50 20

Transient Losses due to Type III ELMs

Type III

	$\delta W\%$	$\delta N\%$
ASDEX Upgrade	0.5 – 2	
DIII-D	1 – 5	
COMPASS-D	1	
TCV	2.5	2

Type II ELMs

- Small energy loss per ELM
- Requires proximity to double null and highly shaped plasmas
- High p_{ped}, (confinement ~like Type I ELMs)
- Low T_e^{ped} (T_{ped}(Type II)~T_{crit}(Type I->III transition))
- Broadband MHD activity
- But for narrow operational window and high n/n_G ~0.5-1
- Type I and Type II often co-exist

Grassy ELMs

- Small ELMs at high confinement mainly seen on JT-60U
- β_p is the critical parameter, although high δ and q_{95} also required



Grassy ELMs - Effect of Toroidal Rotation



Type V ELMs

- Observed on NSTX
- Similar to EDA/HRS (see later) but no mode observed
- High pedestal collisionality, n/n_G> 1
Type I ELMs

Characteristics

Type I ELMs

Observed on many

machines when

P > 1.5-2*P_{LH}

• ELM crash occurs on very

fast timescales, of the order

of 100-300µs

- The pedestal, both n_e and
- T_e build up again, until the

next ELM occurs on a much

longer time scale.



Precursors to Type I ELMs

Type I : (or 'large type III' – COMPASS-D, TCV?)

	п	m	Δr (cm)	f(kHz)	$\tau(\mu s)$
JET?	0 – 4		5	15	100
ASDEX Upgrade	5 – 10	16-15	1 – 2	20 counter (2 frequencies) ? Co*	10 ³
COMPASS-D	3 - 8	(0.4.4)	1 – 2	70-120 (Ohmic) 140-200 (ECRH)	<10 ³
	(4,5)	(9,14)		(93,116)	50
		10-20		50	50

Transient Losses due to Type I ELMs

Type I $\delta W \sim \Delta R^2 p'_{crit}$

	δW %	$\delta N \%$
JET ASDEX Upgrade • Large DIII-D type III? COMPASS-D* TCV* JTF-2M	2 - 9 3 - 6 1 - 7 3 - 4 3 - 12	1 – 5 3 3 - 7 5

Type I ELMs

Thomson scattering (TS)

The comparison of the ELM density collapse at low and high field side indicates that the ELM crash occurs first in the low field-side of the tokamak



ELMs are characterised by ballooning-like behaviour

Type I ELMs

The density perturbation propagates to the inboard side at ~ ion sound speed.



Theory Models

Theory Models

Issues

- Trigger
- Fast non-linear phase
- Exhaust of plasma
- Recovery and repetitive cycle

Outcomes from developing 'understanding'

- Identify regimes with tolerable ELMs
- Suggests control means



Edge pressure gradient

Type I ELM cycle



Pressure gradient (∇P)

- **1.** ∇P rises on transport time scale
- **2.** ∇**P** clamped by high-n ballooning
 - edge current density rises on resistive time scales
- 3. Medium n instability
 - p and j lost until stable again



What triggers the ELM? Type I ELMs

We believe the Type I ELM is triggered by peeling-ballooning modes

 Comparison of linear stability threshold with observed profiles at ELM onset shows good agreement - Note current (j) = 2- shear (s):



ELMs on JET

Linear MHD Theory

Ideal MHD instabilities in the pedestal:

- ballooning modes
- peeling modes

• There are two main drives for ideal MHD instabilities:

- pressure gradient \Rightarrow ballooning modes
- current gradient \Rightarrow kink, or peeling, modes

In the pedestal region, large pressure gradients can build up

- \Rightarrow directly drives ballooning modes
- \Rightarrow drives bootstrap current \Rightarrow kink, or peeling, modes
- Theoretical codes (ELITE, GATO, MISHKA) exist that can scope out the allowed operating regions
- Most modelling employs limiter geometry approximations
- How accurately does this represent the true separatrix geometry?

Stability Trends

Stability if
$$\alpha \left[D - s \Delta'_{Sh} \right] > \frac{Rqs}{B} j_{\Box}$$

$$j_{\Box} = j_{ohmic} + j_{Bootstrap}; j_{Bootstrap} \sim \alpha f(v_{*e})$$

$$\alpha = -(2Rq^2/B^2)(dp/dr);$$

D = $\epsilon \left(1 - \frac{1}{q_a^2}\right) - 'magnetic well'$

Implications

•
$$v_{*_e} \downarrow \Rightarrow j_{Bootstrap} \uparrow \Rightarrow destabilising$$

• current ramp down \Rightarrow stabilising

Different radial mode structures exist in different regimes



Rotation

Flows below sound speed only affect highest mode numbers

- Toroidal flow shear has been incorporated into ELITE (high flow shear, but flow<<sound speed)
- Stabilising effect on the highest *n* modes, but negligible influence on modes responsible for ELMs: sonic flows may have an impact
 - more important in STs, where rotation is higher (and sound speed can approach Alfvén speed)
 - effect of flow shear on non-linear evolution is an open question



Diamagnetic Effects

- do they affect MHD model?

Diamagnetic effects are likely to be important in the pedestal

- predicted to stabilise ballooning modes when

 $\frac{\omega_*}{2} > \gamma \qquad \omega_* = \frac{nq}{2r} \rho_i v_{th,i} \frac{1}{n_i} \frac{dn_i}{dr}$

-usually only gives small quantitative difference in practice



Increasing ω_* \longrightarrow

Huysmans, 2001

Snyder, 2002

Role of Diamagnetic Stabilisation



This becomes

 $\omega_* > 2\gamma$

n=toroidal mode number ε =inverse aspect ratio β_{θ} =poloidal beta ρ_i =ion larmor radius Δ =pedestal width $\omega_A = v_A/Rq$



• Diamagnetic stabilisation of most dangerous $n \sim 10$ modes occurs at higher poloidal β - also a role for q, depending on pedestal scaling with r_i .

– could this explain some small ELM regimes?

Impact of the Separatrix







Type III ELMs

• The mechanism for Type III ELMs is less clear than for Type I:

 Low density Type III ELMs could be peeling: but pure peeling modes are very localised

- High density Type III could be resistive ballooning (below critical T_e): but why an explosive event, rather than diffusive transport?

– could resistive ballooning trigger the peeling mode?

Type III ELMs could also be a consequence of avalanche (e.g. 'sandpile' model) phenomena



Other Type III ELM Theory Models (1)

 Chankin-Saibene resistive ballooning model for triggering Type III ELMs compared with JET data



Fig. 4.12. Pedestal density at the Type I-III ELM transition and during Type III ELMs. (From Ref. [105].)

Other Type III ELM Theory Models (2)

 Pogutse-Igitkhanov resistive interchange model driven by magnetic flutter for triggering Type III ELMs compared with JET data



Fig. 4.11. Pedestal $n_e - T_e$ diagram for 2.5 MA/2.4-2.6T and 3.3-3.6MA/3.4T discharges. $n_{e,ped}$ is measured with the FIR interferometer outermost channel and $T_{e,ped}$ with the ECE heterodyne radiometer. The data are compared with the critical temperature (or upper boundary) for Type III ELMs predicted by the model of Pogutse and Igitkhanov [127,128]. (From Ref. [105].)

Power Expelled in an ELM

Target Energy Deposited due to ELM (JET)



Fig. 7.1. Target energy load due to ELMs, ΔW_{target} , versus energy lost from plasma due to ELMs, ΔW . (From Ref. [214].)

Time Lag to Divertor Target of Main Heat Flux

(Particle-in-cell kinetic calculations show faster high energy electron loss to divertor plates)



Collisionality Dependence of ELM Energy Loss



Fig. 5.4. Normalised ELM energy loss (ΔW_{ELM}/W_{ped}) versus pedestal plasma collisionality for a large range of Type I ELMy H-mode plasmas in ASDEX Upgrade, DIII-D, JT-60U and JET including various plasma triangularities, ratios of P_{INPUT}/P_{L-H}, pellet triggered ELMs, and impurity seeded discharges (Ar). (From Ref. [15].)

Theory input - Peeling-Ballooning modes



Peeling-ballooning Modes

Reduced $\delta W_{\text{ELM}}/W_{\text{ped}}$ at high $n_{e},\,n/n_{G}$ correlated with reduced mode width



Linear Ideal MHD (GATO): Type I vs Type II ELMs



ELM affected area decreases at high q_{95} + high δ for the same pressure profile..

Radial Efflux from ELMs on MAST

TS profiles obtained near ELM peak show broad n_e tail on the outboard



ELMs show D_a emission well beyond outboard separatrix



Large particle flux (J_{SAT}) to outboard mid-plane probe during ELM



Radial efflux observed ~ 1 ELM in 5

The Non-linear Phase

ELM Spatial Structure





Filament structures clearly exist during ELMs but what role do they play in the ELM loss mechanism ?

Filaments Characteristics



The structures appear to

- follow the field lines
- have an extent perpendicular to the field line of ~ 5-10 cm
- toroidal mode number ~10-15
- radial velocities of 400 ms⁻¹ (AUG) and 800 ms⁻¹ (MAST)
- give radial effluxes up to 10 cm (AUG) and 20cm (MAST)

Propagation of the Filaments



Time from start of ELM (µs)

- Decelerate toroidally
- Accelerate radially



Propagation of the Filaments





Time from start of ELM (µs)

- Decelerate toroidally
- Accelerate radially



Radial Propagation of the Filaments



Accelerations ~ 5-15x10⁶ ms⁻²

Accelerations ~ 1.5-6.5x10⁶ ms⁻²

Analytic Theory

- Non-linear models, and experimental data, indicate that the ballooning mode ejects a number (~10) filaments of hot plasma from the pedestal region
- •Analytic theory for high-*n* modes (Cowley & Wilson):
 - a tour de force of algebra, based on a number of approximations:
 - an ordering of spatial scales derived from linear theory
 - close proximity to marginal stability
 - periodicity boundary conditions assumed not to be important
- Predictions include:
 - Ejected explosively from the pedestal
 - The filaments are extended along field lines, but localised toroidally
 - Hot filaments (flux tubes) of plasma are formed




Numerical Studies of Non-linear Evolution JOREK predicts low *n* modes appear to saturate

- Numerical modelling of low-*n* kink modes:
 - Low *n* modes appear to saturate, rather than "explode"
 - Consistent with "outer" mode on JET and quasi-coherent mode of DIII-D

– Could the existence of a saturated low *n* mode then suppress ELMs (eg as in QH-mode)?





Density distribution

Numerical Studies of Non-linear Evolution (S Jardin et al)

Nonlinear 2F ELM Computation with NIMROD

- Project's first large-scale 3D computation with Hall effect and Braginskii gyroviscosity.
- Nonlinear evolution from DIII-D 113317 equilibrium includes toroidal modes $0 \le n \le 42$.
- Linear two-fluid stabilization is obtained for large-n.
- Nonlinear coupling is producing poloidal localization, unlike our previous MHD results.





Number density in the $\phi=0$ plane at simulation time t=82.3 µs has poloidally localized ripples.





Temperature perturbations reach 100 eV at this time (T_{ped} =400 eV) and show a nonlinear helical structure. Perturbed plasma flow vectors are superposed. 20

Numerical Studies of Non-linear Evolution: BOUT confirms explosive nature of intermediate *n* modes

- Numerical modelling of intermediate-*n* modes:
 - Non-linear MHD codes being used to explore explosive behaviour
 - These use more advanced plasma models than the analytic theory, and are not subject to the same approximations
 - There are, of course, numerical limitations
 - BOUT does predict an instability with an explosive nature:



Surface of constant density perturbation



The Post-crash State: Taylor Relaxation Theory

• Gimblett, Hastie and Helander have applied Taylor relaxation model to the pedestal region: by-passes details of the mechanism



- Initial state is marginally peeling unstable
- Triggers the relaxation, minimising energy
 - conserve helicity
 - conserve poloidal flux in annulus
- Current flattens: destabilises peeling
- Skin currents form at boundaries of relaxed region
 - stabilising
- Peeling stability regained when width $\Delta > \Delta_c$ $\Rightarrow \Delta_c$ defines the ELM-affected region
- Predictions (MAST, high collisionality)
 - $-\Delta W_{ELM}/W_{ped}$ ~1%
 - ELM width~few percent
 - large spread, depending on \boldsymbol{q}_a

- To address this question, a non-linear model is essential
- It must address:
 - The rapid, explosive growth of the ELM
 - Why the instability is transient and repetitive, rather than a steady, saturated mode
 - Or, better still, when is it a transient burst of activity and when is it steady, saturated mode?

Transport Code Modelling

- Evolve j, T_e, n with L-H mode transport
- Monitor trajectory in $\,j^{-\alpha}\,$ stability diagram for trigger time
- Simulate losses ${}^{\delta W_{ELM}}$ by enhanced χ_{\perp} over ${}^{\Delta r_{ELM}}$ for time τ_{ELM} , say $\chi_{\perp} \sim 10m^2s^{-1}$ from turbulent transport
- Produces cyclical behaviour
- f_{ELM} given by reheating time

 \Rightarrow need real physics-based models for $\chi_{\perp ELM}$, $\Delta r_{ELM}, \tau_{ELM} \Rightarrow$ non-linear model

Transport Code Modelling of ELM Cycle



ASTRA Simulations of the ELM Cycle

- Fig. A Time evolution of the critical (blue) and total (red dashed) currents at the edge; pedestal electron temperature T_e (green)
- Fig. B Time evolution of the stored pedestal energy ΔW_{ped} (red dashed) and total pressure (blue) at the edge;



Physics Basis for ELM Cycle Modelling

- Trigger linear stability threshold
- **Crash time** $\tau_{\text{ELM}} \sim \tau_{\text{Alfven}} (\tau_{\text{Res}} / \tau_{\text{Alfven}})^{\text{p}}; p \sim 1/3 1$
- Energy loss $\left(\frac{\delta W_{ELM}}{W}\right)_0 \sim \frac{\Delta_{ELM}}{a} \sim \frac{1}{nqs}$
- But only really lost if ideal mode connects to divertor plate $\delta W_{\text{FIM}} = \frac{\delta W_{\text{FIM}}}{1} = \frac{1}{2\pi} - \frac{\pi P_{\text{C}}(1 + M_{\text{FIM}})}{2}$

$$\Rightarrow \frac{\sigma \mathbf{w}_{\text{ELM}}}{W} \sim \left(\frac{\sigma \mathbf{w}_{\text{ELM}}}{W}\right)_0 \frac{1}{1 + \tau_0 / \tau_{\text{ELM}}} \qquad \tau_0 = \pi Rq(1 + \nu_{*e}) / c_s$$

fits data

A Qualitative Analytic Model (Kerner, Pogutse et al)

• Ballooning mode in SOL

- precursor expelling tube
$$\delta_1 \sim L_{px}$$
 in
 $\tau_1 \sim \sqrt{L_{px}R/C_s}$

$$\Rightarrow \frac{\delta W}{W} \sim \frac{L_p^2}{a^2} \frac{P_a}{\langle P \rangle} \sim 10^{-3} : \text{ too small}$$

- Interacts with target plates, filling X-point with impurities
 - acts as effective limiter

$$\Rightarrow$$
 flute instability growing in $\tau_2 \sim \sqrt{L_{pa}R/C_s}$

• Produces Type I ELM, expelling $\Delta_{\text{ELM}} \sim a / nq$

• Refills on
$$\tau_3 \sim \tau_E (\Delta_{ELM} / a)^2$$

•
$$\frac{\delta W_{ELM}}{W} \sim \frac{2}{nq} \frac{p_a}{\langle p \rangle} \sim 5\%$$
 for n=1; $f_{ELM} \propto \frac{P}{\delta W} \propto \frac{BP}{I^3}$ - fits JET data!

• There are three possible contenders

-The filaments act as 'leaky hosepipes': energy and particles diffuse from the hot filaments into the cold SOL: no reconnection required

The filaments act as a conduit, connecting the hot core plasma to the SOL target plates: reconnection is required

-The filaments remove the sheared rotation in the plasma pedestal, which then collapses: no reconnection required

• These are just ideas: all need further work to place on a firm scientific basis

(1) The Leaky Hosepipe Model

• Within the ideal MHD model, a hot flux tube of plasma twists and pushes out between field lines on neighbouring flux surfaces

• If no reconnection occurs, heat can only be lost through diffusion from the filament to the SOL



Pedestal becomes unstable to ballooning



Theory predicts and expt observes filamentation
Filament pushes out into SOL

(2) Filament Reconnection: "Squirting Hosepipe"

- Reconnection would preferentially occur as the filaments cross the Xpoint
 - high magnetic shear would rip the filaments apart
- Flux tubes now connect hot pedestal directly onto SOL target plates
 Different mechanisms for DND and SND: DND ELMs more benign?

SND: Filaments connect target plates via pedestal core plasma
Heat/particles stream to target plates from pedestal

DND: Filaments break off: Could repeat many times during an ELM?

(3) Flow Shear Suppression & Barrier Collapse

- Filaments can only be ejected if flow shear is suppressed
 - suppression of flow shear would lead to enhanced transport
 - barrier would collapse
- Flow shear is suppressed during an ELM, but :
 - does ballooning mode suppress flow shear leading to barrier collapse?

– Or does something else suppress flow shear, allowing ballooning modes to grow? MAST
 DIII-D



A Kirk, et al, PPCF 2005

Boedo, et al, Phys Plas 2005

- We have the tools to study the non-linear evolutions, but they need more development
- Analytic theory provides simplified non-linear equations, but no final answer yet:
 - coefficients need to be determined

 sign of quadratic non-linearity determines whether filament goes in or out

requires an efficient solution of non-linear equation for parameter scans

non-trivial due to finite time singularity and fractional derivatives

- We are making progress here
- Numerical studies qualitatively confirm the analytic predictions for intermediate *n*, but more work is needed:
 - unable to produce the full ELM cycle from first-principles
 - what is the saturation mechanism?
 - what is the dominant transport mechanism?

ELM Control

Active ELM Control Techniques

- ELM Control using magnetic coils
- ELM pacemaking using pellets
- Toroidal ripple

ELM Control using Magnetic Coils

- Stochastic Layer ELM Control on DIII-D
- Application of n=3 perturbation dramatically changes

the character of the edge recycling.



ELM Control using Magnetic Coils

Dramatic reduction in ELM energy losses



ELM Control using Pellet Pace Making

- Pioneered on AUG
- ELMs are triggered by each pellet



Effect of Toroidal Ripple

In JT-60U the energy loss due to most of type I ELMs is

less than ~6% of W_{ped}

- Thought to be due to the large toroidal ripple
- The downside is the poorer energy confinement time



Stationary ELM-Free H-Mode

Regimes

Stationary ELM-Free H-Mode Regimes

- EDA: Enhanced D-Alpha
- QH-mode: Quiescent H-mode
- HRS: High Recycling Steady H-mode

EDA Mode

- First seen on CMOD
- Observed at high density and low to modest heating power
- Observed at high edge
- collisionality $n_{95}/n_G > \sim 1.5$
- Global confinement can be as

good as in Type I ELMy regimes.

ALCATOR C-Mod

D Mossessian, PoP **10** (2003) 1720



EDA Mode

- Density kept constant due to the existence of a quasicoherent (QC) mode (50-120 Khz range high n,m) In similarity experiments AUG and
- DIII-D have seen a QC
- but have not established
- a steady state regime



Q-H Mode

- First seen on DIII-D robustly
 reproduced on AUG
- Only observed in counter NBI with a large plasma wall distance (suggesting a role of fast ions)
- Low density regime ($n_e/n_G \sim$
- 0.04) pedestal pressures
- comparable to Type I ELMy H-





Q-H Mode

Edge Harmonic Oscillation typically observed, non sinusoidal mode giving a mix of toroidal mode numbers (n=1,2,3,4,..., f(n=1) 5-11 kHz). Possibly accompanied by a HFO (350-500 kHz)



HRS Mode

- First seen on JFT-2M
- Very similar to EDA
- Access favours high

density and neutral

pressure.

- High edge collisionality
- High frequency (>100

kHz) edge modes

observed.



 Type I ELMs are triggered by ideal MHD peeling-ballooning modes

Most ELMs seem to be associated with filamentary structures

• Flow shear is suppressed during an ELM

- The plasma current density plays an important role

 high plasma current density results in large ELMs
- Toroidal flows need to approach sonic speeds to have an impact on ELM trigger: what about the impact on the non-linear evolution?
- Diamagnetic effects are important at the edge, reducing growth rates – plasmas with strong diamagnetic effects may have smaller ELMs (high β_{θ}, q)
- There seems to be a correlation between ELM size and linear eigenmode width

 ELM affected area not always determined by eigenmode, but sometimes is

 Ergodising magnetic field in pedestal can hold gradients below stability threshold: suppresses ELMs

Summary: What we don't know

- The implications of separatrix geometry is not clear
 - is the ideal MHD peeling mode stabilised? Seems to be
 - a resistive peeling mode is predicted
 - what is the impact of open field lines of the SOL?
- Is current ejected during the ELM: what mechanism, and how fast?
- While filaments are associated with ELMs, are they a cause or an effect?
- If the cause, how do they lead to heat loss?
 - suppression of shear flow in barrier?
 - act as a tube, connecting pedestal to SOL?
 - is reconnection important?
- In the no-ELM regimes (QH and EDA mode), what suppresses ELMs?
- What is the mechanism behind the pellet-triggered ELMs?
 Why are they smaller?
- What is the key ingredient to achieve small ELMs?

Final Summary

 Many different ELMing and ELM free regimes exist – most are not ITER relevant – but do increase our understanding

• The Type I ELM regime is the basis for ITER operation – there are potential ways to decrease their impact onto plasma facing components

• The more we can understand about the ELM the easier it is to make quantitative predictions for future devices

• A predictive ELM model is critically needed